





# Data-driven prediction of battery cycle life before capacity degradation

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**Accurately predicting the lifetime of complex, nonlinear systems such as lithium-ion batteries is critical for accelerating technology development. However, diverse aging mechanisms, significant device variability and dynamic operating conditions have remained major challenges. We generate a comprehensive dataset consisting of 124 commercial lithium iron phosphate/graphite cells cycled under fast-charging conditions, with widely varying cycle lives ranging from 150 to 2,300 cycles. Using discharge voltage curves from early cycles yet to exhibit capacity degradation, we apply machine-learning tools to both predict and classify cells by cycle life. Our best models achieve 9.1% test error for quantitatively predicting cycle life using the first 100 cycles (exhibiting a median increase of 0.2% from initial capacity) and 4.9% test error using the first 5 cycles for classifying cycle life into two groups. This work highlights the promise of combining deliberate data generation with data-driven modelling to predict the behaviour of complex dynamical systems.**

Lithium-ion batteries are deployed in a wide range of applications due to their low and falling costs, high energy densities and long lifetimes<sup>1–3</sup>. However, as is the case with many chemical, mechanical and electronic systems, long battery lifetime entails delayed feedback of performance, often many months to years. Accurate prediction of lifetime using early-cycle data would unlock new opportunities in battery production, use and optimization. For example, manufacturers can accelerate the cell development cycle, perform rapid validation of new manufacturing processes and sort/grade new cells by their expected lifetime. Likewise, end users could estimate their battery life expectancy<sup>4–6</sup>. One emerging application enabled by early prediction is high-throughput optimization of processes spanning large parameter spaces (Supplementary Figs. 1 and 2), such as multistep fast charging and formation cycling, which are otherwise intractable due to the extraordinary time required. The task of predicting lithium-ion battery lifetime is critically important given its broad utility but challenging due to nonlinear degradation with cycling and wide variability, even when controlling for operating conditions<sup>7–11</sup>.

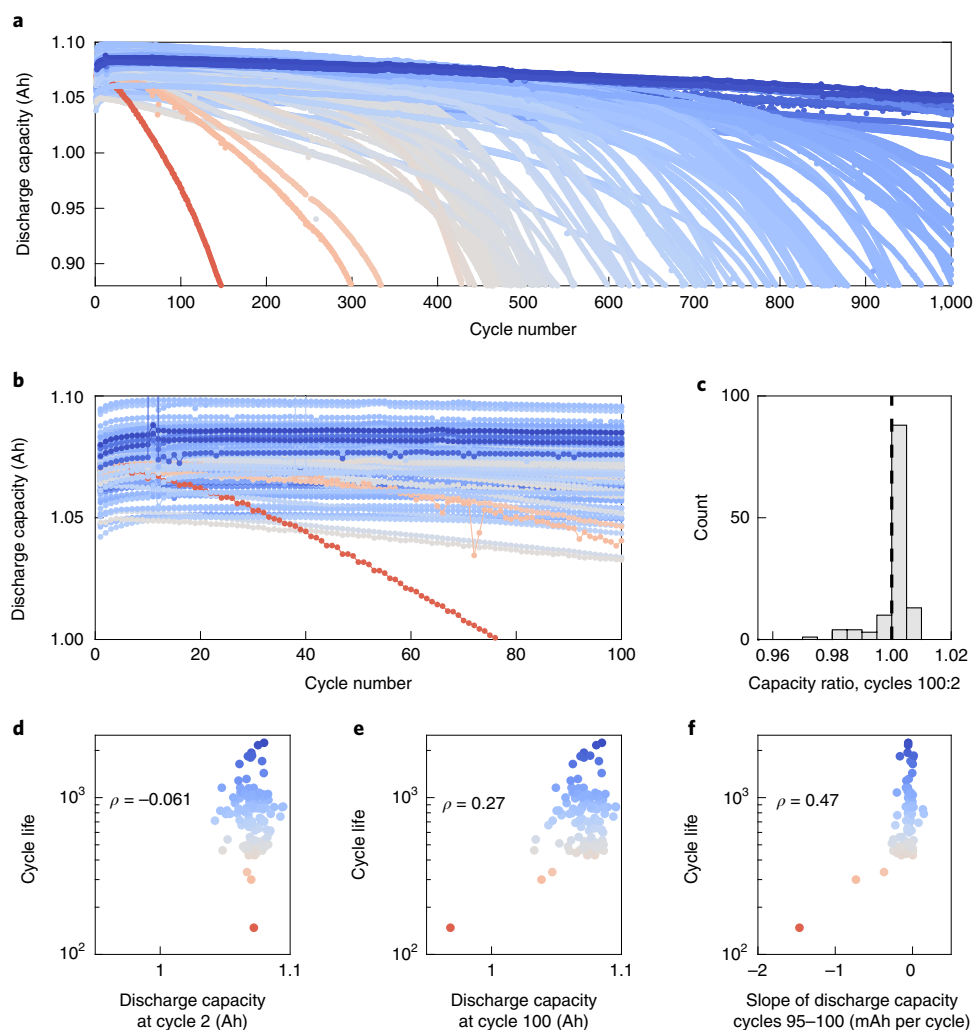
Many previous studies have modelled lithium-ion battery lifetime. Bloom et al.<sup>12</sup> and Broussely et al.<sup>13</sup> performed early work that fitted semi-empirical models to predict power and capacity loss. Since then, many authors have proposed physical and semi-empirical models that account for diverse mechanisms such as growth of the solid–electrolyte interphase<sup>14,15</sup>, lithium plating<sup>16,17</sup>, active material loss<sup>18,19</sup> and impedance increase<sup>20–22</sup>. Predictions of remaining useful life in battery management systems, summarized in these reviews<sup>5,6</sup>, often rely on these mechanistic and semi-empirical models for state estimation. Specialized diagnostic measurements such as coulombic efficiency<sup>23,24</sup> and impedance spectroscopy<sup>25–27</sup> can also be used for lifetime estimation. While these chemistry and/or mechanism-specific models have shown predictive success, developing models that describe full cells cycled under relevant operating

conditions (for example, fast charging) remains challenging, given the many degradation modes and their coupling to thermal<sup>28,29</sup> and mechanical<sup>28,30</sup> heterogeneities within a cell<sup>30–32</sup>.

Approaches using statistical and machine-learning techniques to predict cycle life are attractive, mechanism-agnostic alternatives. Recently, advances in computational power and data generation have enabled these techniques to accelerate progress for a variety of tasks, including prediction of material properties<sup>33,34</sup>, identification of chemical synthesis routes<sup>35</sup> and material discovery for energy storage<sup>36–38</sup> and catalysis<sup>39</sup>. A growing body of literature<sup>6,40,41</sup> applies machine-learning techniques for predicting the remaining useful life of batteries using data collected in both laboratory and online environments. Generally, these works make predictions after accumulating data corresponding to degradation of at least 25% along the trajectory to failure<sup>42–48</sup> or using specialized measurements at the beginning of life<sup>11</sup>. Accurate early prediction of cycle life with significantly less degradation is challenging because of the typically nonlinear degradation process (with negligible capacity degradation in early cycles) as well as the relatively small datasets used to date that span a limited range of lifetimes<sup>49</sup>. For example, Harris et al.<sup>10</sup> found a weak correlation ( $\rho=0.1$ ) between capacity values at cycle 80 and capacity values at cycle 500 for 24 cells exhibiting nonlinear degradation profiles, illustrating the difficulty of this task. Machine-learning approaches are especially attractive for high-rate operating conditions, where first-principles models of degradation are often unavailable. In short, opportunities for improving upon state-of-the-art prediction models include higher accuracy, earlier prediction, greater interpretability and broader application to a wide range of cycling conditions.

In this work, we develop data-driven models that accurately predict the cycle life of commercial lithium iron phosphate (LFP)/graphite cells using early-cycle data, with no prior knowledge of degradation mechanisms. We generated a dataset of 124 cells with

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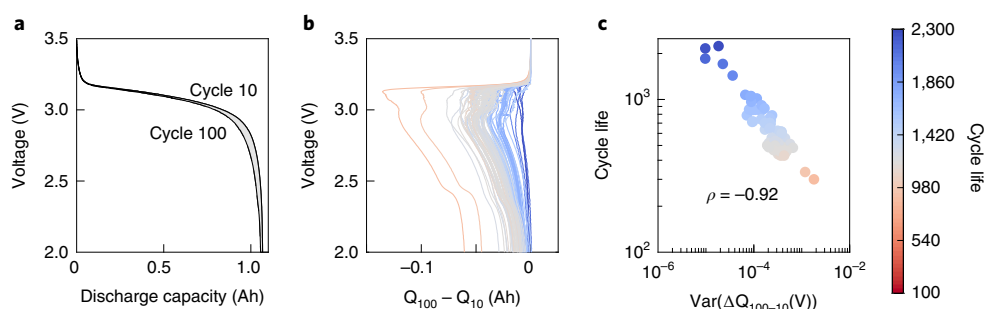
**Fig. 1 | Poor predictive performance of features based on discharge capacity in the first 100 cycles.** **a**, Discharge capacity for the first 1,000 cycles of LFP/graphite cells. The colour of each curve is scaled by the battery's cycle life, as is done throughout the manuscript. **b**, A detailed view of **a**, showing only the first 100 cycles. A clear ranking of cycle life has not emerged by cycle 100. **c**, Histogram of the ratio between the discharge capacity of cycle 100 and that of cycle 2. The cell with the highest degradation (90%) is excluded to show the detail of the distribution. The dotted line indicates a ratio of 1.00. Most cells have a slightly higher capacity at cycle 100 relative to cycle 2. **d**, Cycle life as a function of discharge capacity at cycle 2. The correlation coefficient of capacity at cycle 2 and log cycle life is  $-0.06$  (remains unchanged on exclusion of the shortest-lived battery). **e**, Cycle life as a function of discharge capacity at cycle 100. The correlation coefficient of capacity at cycle 100 and log cycle life is  $0.27$  ( $0.08$  excluding the shortest-lived battery). **f**, Cycle life as a function of the slope of the discharge capacity curve for cycles 95–100. The correlation coefficient of this slope and log cycle life is  $0.47$  ( $0.36$  excluding the shortest-lived battery).

cycle lives ranging from 150 to 2,300 using 72 different fast-charging conditions, with cycle life (or equivalently, end of life) defined as the number of cycles until 80% of nominal capacity. For quantitatively predicting cycle life, our feature-based models can achieve prediction errors of 9.1% using only data from the first 100 cycles, at which point most batteries have yet to exhibit capacity degradation. Furthermore, using data from the first 5 cycles, we demonstrate classification into low- and high-lifetime groups and achieve a misclassification test error of 4.9%. These results illustrate the power of combining data generation with data-driven modelling to predict the behaviour of complex systems far into the future.

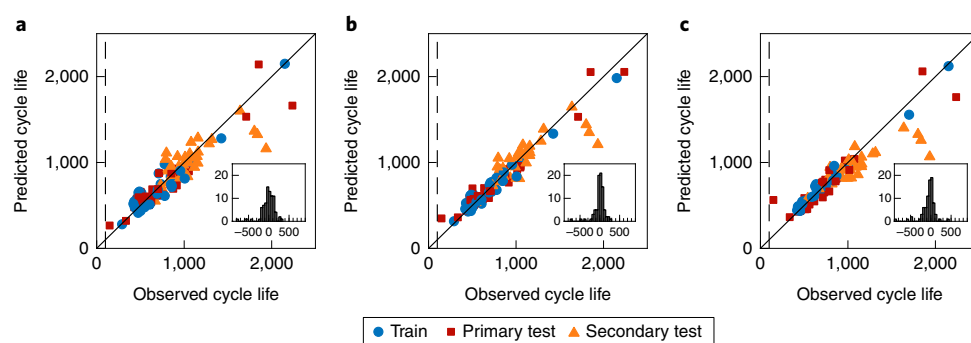
### Data generation

We expect the space that parameterizes capacity fade in lithium-ion batteries to be high dimensional due to their many capacity fade mechanisms and manufacturing variability. To probe this space, commercial LFP/graphite cells (A123 Systems, model

APR18650M1A, 1.1 Ah nominal capacity) were cycled in a temperature-controlled environmental chamber (30 °C) under varied fast-charging conditions but identical discharging conditions (4 C to 2.0 V, where 1 C is 1.1 A; see Methods for details). Since the graphite negative electrode dominates degradation in these cells, these results could be useful for other lithium-ion batteries based on graphite<sup>32,50–54</sup>. We probe average charging rates ranging from 3.6 C, the manufacturer's recommended fast-charging rate, to 6 C to probe the performance of current-generation power cells under extreme fast-charging conditions (~10 min charging), an area of significant commercial interest<sup>55</sup>. By deliberately varying the charging conditions, we generate a dataset that captures a wide range of cycle lives, from approximately 150 to 2,300 cycles (average cycle life of 806 with a standard deviation of 377). While the chamber temperature is controlled, the cell temperatures vary by up to 10 °C within a cycle due to the large amount of heat generated during charge and discharge. This temperature variation is a function of



**Fig. 2 | High performance of features based on voltage curves from the first 100 cycles.** **a**, Discharge capacity curves for 100th and 10th cycles for a representative cell. **b**, Difference of the discharge capacity curves as a function of voltage between the 100th and 10th cycles,  $\Delta Q_{100-10}(V)$ , for 124 cells. **c**, Cycle life plotted as a function of the variance of  $\Delta Q_{100-10}(V)$  on a log-log axis, with a correlation coefficient of  $-0.93$ . In all plots, the colours are determined based on the final cycle lifetime. In **c**, the colour is redundant with the y-axis. In **b** and **c**, the shortest lived battery is excluded.



**Fig. 3 | Observed and predicted cycle lives for several implementations of the feature-based model.** The training data are used to learn the model structure and coefficient values. The testing data are used to assess generalizability of the model. We differentiate the primary test and secondary test datasets because the latter was generated after model development. The vertical dotted line indicates when the prediction is made in relation to the observed cycle life. The inset shows the histogram of residuals (predicted - observed) for the primary and secondary test data. **a**, 'Variance' model using only the log variance of  $\Delta Q_{100-10}(V)$ . **b**, 'Discharge' model using six features based only on discharge cycle information, described in Supplementary Table 1. **c**, 'Full' model using the nine features described in Supplementary Table 1. Because some temperature probes lost contact during experimentation, four cells are excluded from the full model analysis.

internal impedance and charging policy (Supplementary Figs. 3 and 4). Voltage, current, cell can temperature and internal resistance are continuously measured during cycling (see Methods for additional experimental details). The dataset contains approximately 96,700 cycles; to the best of the authors' knowledge, our dataset is the largest publicly available for nominally identical commercial lithium-ion batteries cycled under controlled conditions (see Data availability section for access information).

Fig. 1a,b shows the discharge capacity as a function of cycle number for the first 1,000 cycles, where the colour denotes cycle life. The capacity fade is negligible in the first 100 cycles and accelerates near the end of life, as is often observed in lithium-ion batteries. The crossing of the capacity fade trajectories illustrates the weak relationship between initial capacity and lifetime; indeed, we find weak correlations between the log of cycle life and the discharge capacity at the second cycle ( $\rho = -0.06$ , Fig. 1d) and the 100th cycle ( $\rho = 0.27$ , Fig. 1e), as well as between the log of cycle life and the capacity fade rate near cycle 100 ( $\rho = 0.47$ , Fig. 1f). These weak correlations are expected because capacity degradation in these early cycles is negligible; in fact, the capacities at cycle 100 increased from the initial values for 81% of cells in our dataset (Fig. 1c). Small increases in capacity after a slow cycle or rest period are attributed to charge stored in the region of the negative electrode that extends beyond the positive electrode<sup>56,57</sup>. Given the limited predictive power of these correlations based on the capacity

fade curves, we employ an alternative data-driven approach that considers a larger set of cycling data including the full voltage curves of each cycle, as well as additional measurements including cell internal resistance and temperature.

### Machine-learning approach

We use a feature-based approach to build an early-prediction model. In this paradigm, features, which are linear or nonlinear transformations of the raw data, are generated and used in a regularized linear framework, the elastic net<sup>58</sup>. The final model uses a linear combination of a subset of the proposed features to predict the logarithm of cycle life. Our choice of a regularized linear model allows us to propose domain-specific features of varying complexity while maintaining high interpretability. Linear models also have low computational cost; the model can be trained offline, and online prediction requires only a single dot product after data preprocessing.

We propose features from domain knowledge of lithium-ion batteries (though agnostic to chemistry and degradation mechanisms), such as initial discharge capacity, charge time and cell can temperature. To capture the electrochemical evolution of individual cells during cycling, several features are calculated based on the discharge voltage curve (Fig. 2a). Specifically, we consider the cycle-to-cycle evolution of  $Q(V)$ , the discharge voltage curve as a function of voltage for a given cycle. As the voltage range is identical for every cycle, we consider capacity as a function of voltage, as

**Table 1 | Model metrics for the results shown in Fig. 3**

	RMSE (cycles)			Mean percent error (%)		
	Train	Primary test	Secondary test	Train	Primary test	Secondary test
'Variance' model	103	138 (138)	196	14.1	14.7 (13.2)	11.4
'Discharge' model	76	91 (86)	173	9.8	13.0 (10.1)	8.6
'Full' model	51	118 (100)	214	5.6	14.1 (7.5)	10.7

Train and primary/secondary test refer to the data used to learn the model and evaluate model performance, respectively. One battery in the test set reaches 80% state-of-health rapidly and does not match other observed patterns. Therefore, the parenthetical primary test results correspond to the exclusion of this battery.

opposed to voltage as a function of capacity, to maintain a uniform basis for comparing cycles. For instance, we can consider the change in discharge voltage curves between cycles 20 and 30, denoted  $\Delta Q_{30-20}(V) = Q_{30}(V) - Q_{20}(V)$ , where the subscripts indicate cycle number. This transformation,  $\Delta Q(V)$ , is of particular interest because voltage curves and their derivatives are a rich data source that is effective in degradation diagnosis<sup>50,51,53,59-64</sup>.

The  $\Delta Q(V)$  curves for our dataset are shown in Fig. 2b using the 100th and 10th cycles, that is,  $\Delta Q_{100-10}(V)$ . We discuss our selection of these cycle numbers at a later point. Summary statistics, for example minimum, mean and variance, were then calculated for the  $\Delta Q(V)$  curves of each cell. Each summary statistic is a scalar quantity that captures the change in voltage curves between two cycles. In our data-driven approach, these summary statistics are selected for their predictive ability, not their physical meaning. Immediately, a clear trend emerges between cycle life and a summary statistic, specifically variance, applied to  $\Delta Q_{100-10}(V)$  (Fig. 2c).

Because of the high predictive power of features based on  $\Delta Q_{100-10}(V)$ , we investigate three different models using (1) only the variance of  $\Delta Q_{100-10}(V)$ , (2) additional candidate features obtained during discharge and (3) features from additional data streams such as temperature and internal resistance. In all cases, data were taken only from the first 100 cycles. These three models, each with progressively more candidate features, were chosen to evaluate both the cost-benefit of acquiring additional data streams and the limits of prediction accuracy. The training data (41 cells) are used to select the model features and set the values of the coefficients, and the primary testing data (43 cells) are used to evaluate the model performance. We then evaluate the model on a secondary testing dataset (40 cells) generated after model development. Two metrics, defined in the 'Machine-learning model development' section, are used to evaluate our predictive performance: root-mean-squared error (RMSE), with units of cycles, and average percentage error.

### Performance of early prediction models

We present three models to predict cycle life using increasing candidate feature set sizes; the candidate features are detailed in Supplementary Table 1 and Supplementary Note 1. The first model, denoted as the 'variance' model, does not consider subset selection and uses only the log variance of  $\Delta Q_{100-10}(V)$  for prediction. Surprisingly, using only this single feature results in a model with approximately 15% average percentage error on the primary test dataset and approximately 11% average percentage error on the secondary test dataset. We stress the error metrics of the secondary test dataset, as these data had not been generated at the time of model development and are thus a rigorous test of model performance. The second, 'discharge' model, considers additional information derived from measurements of voltage and current during discharge in the first 100 cycles (row blocks 1 and 2 of Supplementary Table 1). Of 13 features, 6 were selected. Finally, the third, 'full' model considers all available features (all rows blocks of Supplementary Table 1). In this model, 9 out of 20 features were selected (Supplementary Fig. 5). As expected, by adding additional features,

**Table 2 | Model metrics for the classification setting with a cycle life threshold of 550 cycles**

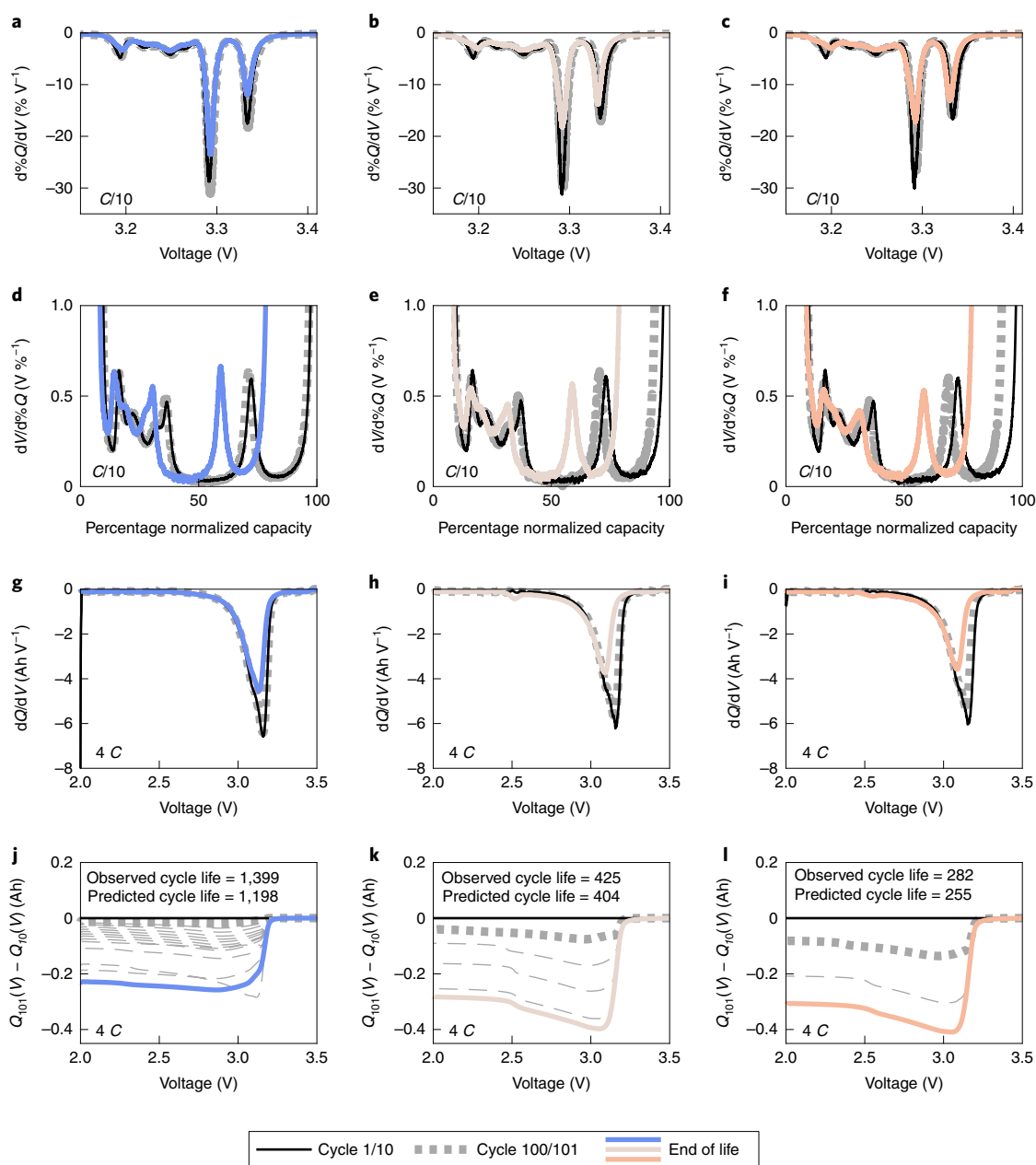
	Classification accuracy (%)		
	Train	Primary test	Secondary test
Variance classifier	82.1	78.6	97.5
Full classifier	97.4	92.7	97.5

Train and primary/secondary test refer to the data used to learn the model and evaluate model performance, respectively.

the primary test average percentage error decreases to 7.5% and the secondary test average percentage error decreases slightly to 10.7%. The error for the secondary test set is slightly higher for the full model when compared with the discharge model (Supplementary Note 2 and Supplementary Figs. 6–7). In all cases, the average percentage error is less than 15% and decreases to as little as 7.5% in the full model, excluding an anomalous cell. Table 1 and Fig. 3 display the performance of the 'variance', 'discharge' and 'full' models applied to our three datasets.

We benchmark the performance of our cycle life prediction using early-cycle data against both prior literature and naïve models. A relevant metric is the extent of degradation that has to occur before an accurate prediction can be made. In our work, accurate prediction was achieved using voltage curves from early cycles corresponding to a capacity increase of 0.2% (median) relative to initial values (with the first and third quartile percentiles being 0.06% and 0.34%, respectively; see Fig. 1c). We are unaware of previous early-prediction demonstrations that do not require degradation in the battery capacity or specialized measurements. In fact, published models<sup>42-48</sup> generally require data corresponding to at least 25% capacity degradation before making predictions at an accuracy comparable to that of this work. We also benchmark our model performance using naïve models, for example univariate models and/or models that only utilize information from the capacity fade curve (Supplementary Note 3, Supplementary Figs. 8–13 and Supplementary Tables 2–3). Notably, if the average cycle life of the training data is used for prediction, the average percentage error is approximately 30% and 36% for the primary and secondary test sets, respectively. Using data from the first 100 cycles, the most complex benchmark model using only features from the discharge capacity fade curve has errors of 23% and 50% for the primary and secondary test sets, respectively. In fact, a similar model that uses discharge capacity fade curve data from the first 300 cycles achieves comparable performance (27% and 46% for the primary and secondary test data, respectively), highlighting the difficulty of prediction without using voltage features.

We also consider contexts in which predictions are required at very low cycle number but the accuracy requirements are less stringent, such as sorting/grading and pack design applications. As an example, we develop a logistic regression model to classify cells into



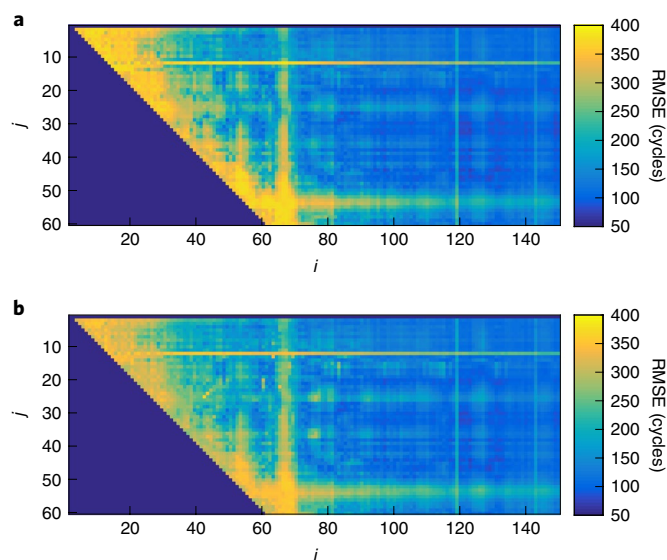
**Fig. 4 | Transformations of voltage–capacity discharge curves for three fast-charged cells that were tested with periodic slow diagnostic cycles.**

**a–c**,  $dQ/dV$  at  $C/10$ ; **d–f**,  $dV/dQ$  at  $C/10$ ; **g–i**,  $dQ/dV$  at  $4C$ ; **j–l**,  $\Delta Q(V)$  at  $4C$ . **a,d,g,j**,  $4C/4C$ ; **b,e,h,k**,  $6C/4C$ ; **c,f,i,l**,  $8C/4C$ . The solid black line is the first cycle (cycle 10 for fast cycling), the dotted grey line is cycle 101 or 100 (fast and slow, respectively) and the coloured thick line is the end-of-life cycle (80% state-of-health). The colour of the end-of-life cycle is consistent with the colour scale in Figs. 1 and 2. For  $\Delta Q(V)$ , a thin dotted grey line is added every 100 cycles. The patterns observed using slow cycling are consistent with  $LAM_{deNE}$  and loss of lithium inventory (Supplementary Fig. 18). The features are smeared during fast charging. The log variance  $\Delta Q(V)$  model dataset predicts the lifetime of these cells within 15%.

either a ‘low-lifetime’ or a ‘high-lifetime’ group, using only the first five cycles for various cycle life thresholds. For the ‘variance classifier’, we use only the  $\Delta Q(V)$  variance feature between the fourth and fifth cycles,  $\text{var}(\Delta Q_{5-4}(V))$ , and attain a test classification accuracy of 88.8%. For the ‘full classifier’, we use regularized logistic regression with 18 candidate features to achieve a test classification accuracy of 95.1%. These results are summarized in Table 2 and detailed in Supplementary Note 4, Supplementary Fig. 14–17 and Supplementary Tables 4–6. This approach illustrates the predictive ability of  $\Delta Q(V)$  even if data from the only first few cycles are used, and, more broadly, showcases our flexibility to tailor data-driven models to various use cases.

### Rationalization of predictive performance

While models that include features from all available data streams generally have the lowest errors, our predictive ability primary comes from features based on transformations of the voltage curves, as evidenced by the performance of the single-feature ‘variance’ model. This feature is consistently selected in both models with feature selection (‘discharge’ and ‘full’). Other transformations of the voltage curves can also be used to predict cycle life; for example, the full model selects both the minimum and variance of  $\Delta Q_{100-10}(V)$ . In particular, the physical meaning of the variance feature is associated with the dependence of the discharged energy dissipation on voltage, which is indicated by the grey region between the voltage



**Fig. 5 | Prediction error as a function of cycle indices.** RMSE error, in units of cycles, is presented for training (a) and testing (b) datasets using only the log variance of  $\Delta Q_{i,j}(V)$ , where indices  $i$  and  $j$  are varied. These errors are averaged over 20 random partitions of the data into equal training and testing datasets. The errors are relatively flat after cycle 80. The increases in error around cycles  $j=55$  and  $i=70$  are due to temperature fluctuations of the environmental chamber (see Supplementary Fig. 25).

curves in Fig. 2a. The integral of this region is the total change in energy dissipation between cycles under galvanostatic conditions and is linearly related to the mean of  $\Delta Q(V)$ . Zero variance would indicate energy dissipations that are independent of voltage. Thus, the variance of  $\Delta Q(V)$  reflects the extent of non-uniformity in the energy dissipation with voltage, due to either open-circuit or kinetic processes, a point that we return to later.

We observe that features derived from early-cycle discharge voltage curves have excellent predictive performance, even before the onset of capacity fade. We rationalize this observation by investigating degradation modes that do not immediately result in capacity fade yet still manifest in the discharge voltage curve and are also linked to rapid capacity fade near the end of life.

While our data-driven approach has successfully revealed predictive features from early-cycle discharge curves, identification of degradation modes using only high-rate data is challenging because of the convolution of kinetics with open-circuit behaviour. Thus, we turn to established methods for mechanism identification using low-rate cycling data. Dubarry et al.<sup>61</sup> mapped degradation modes in LFP/graphite cells to their resultant shift in  $dQ/dV$  and  $dV/dQ$  derivatives for diagnostic cycles at  $C/20$ . One degradation mode—loss of active material of the delithiated negative electrode (LAM<sub>deNE</sub>)—results in a shift in discharge voltage with no change in capacity. This behaviour is observed when the negative electrode capacity is larger than that of the positive electrode, as is the case in these LFP/graphite cells. Thus, a loss of delithiated negative electrode material changes the potentials at which lithium ions are stored without changing the overall capacity<sup>50,61</sup>. As proposed by Anseán et al.<sup>50</sup>, at high rates of LAM<sub>deNE</sub>, the negative electrode capacity will eventually fall below the remaining lithium-ion inventory. At this point, the negative electrode will not have enough sites to accommodate lithium ions during charging, inducing lithium plating<sup>50</sup>. Since plating is an additional source of irreversibility, the capacity loss accelerates. Thus, in early cycles, LAM<sub>deNE</sub> shifts the voltage curve without affecting the capacity fade curve and induces rapid capacity fade at high cycle number. This degradation mode,

in conjunction with loss of lithium inventory, is widely observed in commercial LFP/graphite cells operated under similar conditions<sup>32,50–54</sup>. We note that the graphitic negative electrode is common to nearly all commercial lithium-ion batteries in use today.

To investigate the contribution of LAM<sub>deNE</sub>, we perform additional experiments for cells cycled with varied charging rates (4C, 6C and 8C) and a constant discharge rate (4C), incorporating slow cycling at the 1st, 100th and end-of-life cycles. Derivatives of diagnostic discharge curves at  $C/10$  (Fig. 4, rows 1 and 2) are compared with these, and  $\Delta Q(V)$ , at 4C at the 10th, 101st and end-of-life cycles (rows 3 and 4). The shifts in  $dQ/dV$  and  $dV/dQ$  in diagnostic cycling correspond to a shift of the potentials at which lithium is stored in graphite during charging and are consistent with LAM<sub>deNE</sub> and loss of lithium inventory operating concurrently (Supplementary Fig. 18)<sup>50,51,61</sup>. The magnitude of these shifts from the 1st to 100th cycle increases with charging rate (Supplementary Note 5 and Supplementary Fig. 19). These observations rationalize why models using features based on discharge curves have lower errors than models using only features based on capacity fade curves, since LAM<sub>deNE</sub> does not manifest in capacity fade in early cycles. We note that LAM<sub>deNE</sub> alters a fraction of, rather than the entire, discharge voltage curve, consistent with the strong correlation between the variance of  $\Delta Q(V)$  and cycle life (Fig. 2c). In summary, we attribute the success of our predictive models to features that capture changes in both the capacity fade curves and voltage curves, since degradation may be silent in discharge capacity but present in voltage curves.

As noted above, differential methods such as  $dQ/dV$  and  $dV/dQ$  are used extensively to pinpoint degradation mechanisms<sup>50,51,53,59–61</sup>. These approaches require low-rate diagnostic cycles, as higher rates smear out features due to heterogeneous de(inter)calation<sup>32</sup>, as seen by comparing row 1 with row 3 in Fig. 4. However, these diagnostic cycles often induce a temporary capacity recovery, commonly observed in cells when the geometric area of the negative electrode exceeds that of the positive electrode<sup>56,57</sup>. As such, they interrupt the trajectory of capacity fade (Supplementary Fig. 20). Therefore, by applying summary statistics to  $\Delta Q(V)$  collected at high rate, we simultaneously avoid both low-rate diagnostic cycles and numerical differentiation, which decreases the signal-to-noise ratio<sup>65</sup>. However, these high-rate discharge voltage curves can additionally reflect both kinetic degradation modes and heterogeneities that are not observed in  $dQ/dV$  and  $dV/dQ$  curves at  $C/10$ . We consider the influence of kinetic degradation modes in Supplementary Note 6, Supplementary Fig. 21 and Supplementary Tables 7–8); briefly, we estimate that low-rate modes such as LAM<sub>deNE</sub> primarily contribute (50–80%) to  $\Delta Q(V)$ . We also mention that low-rate degradation modes such as LAM<sub>deNE</sub> influence the kinetics at high rate, in this case by increasing the local current density of the active regions.

Finally, additional analysis was performed to understand the impact of the cycle indices chosen for  $\Delta Q(V)$  features in the regression setting. Univariate linear models using only the variance of  $Q_i(V) - Q_j(V)$  for the training and primary testing datasets were investigated and are displayed in Fig. 5. We find that the model is relatively insensitive to the indexing scheme for  $i > 60$ , suggesting that quantitative cycle life prediction using even earlier cycles is possible. This trend is further validated by the model coefficients shown in Supplementary Fig. 22. We hypothesize that the insensitivity of the model to the indexing scheme implies linear degradation with respect to cycle number, which is often assumed for LAM modes<sup>50,61</sup>. Relative indexing schemes based on cycles in which a specified capacity fade was achieved were also investigated and did not result in improved predictions. Furthermore, because the discharge capacity initially increases, specified decreases in capacity require more cycles to develop than fixed indexing (Supplementary Note 7 and Supplementary Figs. 23–25).

## Conclusions

Data-driven modelling is a promising route for diagnostics and prognostics of lithium-ion batteries and enables emerging applications in their development, manufacturing and optimization. We develop cycle life prediction models using early-cycle discharge data yet to exhibit capacity degradation, generated from commercial LFP/graphite batteries cycled under fast-charging conditions. In the regression setting, we obtain a test error of 9.1% using only the first 100 cycles; in the classification setting, we obtain a test error of 4.9% using data from the first 5 cycles. This level of accuracy is achieved by extracting features from high-rate discharge voltage curves as opposed to only from the capacity fade curves, and without using data from slow diagnostic cycles or assuming prior knowledge of cell chemistry and degradation mechanisms. The success of the model is rationalized by demonstrating consistency with degradation modes that do not manifest in capacity fade during early cycles but impact the voltage curves. In general, our approach can complement approaches based on physical and semi-empirical models and on specialized diagnostics. Broadly speaking, this work highlights the promise of combining data generation and data-driven modelling for understanding and developing complex systems such as lithium-ion batteries.

## Methods

**Cell cycling and data generation.** 124 commercial high-power LFP/graphite A123 APR18650M1A cells were used in this work. The cells have a nominal capacity of 1.1 Ah and a nominal voltage of 3.3 V. The manufacturer's recommended fast-charging protocol is 3.6 C constant current–constant voltage (CC-CV). The rate capability of these cells during charge and discharge is shown in Supplementary Fig. 27.

All cells were tested in cylindrical fixtures with four-point contacts on a 48-channel Arbin LBT battery testing cycle. The tests were performed at a constant temperature of 30 °C in an environmental chamber (Amerex Instruments). Cell can temperatures were recorded by stripping a small section of the plastic insulation and contacting a type T thermocouple to the bare metal casing using thermal epoxy (OMEGATHERM 201) and Kapton tape.

The cells were cycled with various candidate fast-charging policies (Supplementary Table 9) but identically discharged. Cells were charged from 0% to 80% state-of-charge (SOC) with one of 72 different one-step and two-step charging policies. Each step is a single C rate applied over a given SOC range; for example, a two-step policy could consist of a 6 C charging step from 0% to 50% SOC, followed by a 4 C step from 50% to 80% SOC. The 72 charging policies represent different combinations of current steps within the 0% to 80% SOC range. The charging time from 0% to 80% SOC ranged from 9 to 13.3 min. An internal resistance measurement was obtained during charging at 80% SOC by averaging 10 pulses of  $\pm 3.6$  C with a pulse width of 30 or 33 ms, where 1 C is 1.1 A, or the current required to fully (dis)charge the nominal capacity (1.1 Ah) in 1 h. All cells then charged from 80% to 100% SOC with a uniform 1 C CC-CV charging step to 3.6 V and a current cutoff of C/50. All cells were subsequently discharged with a CC-CV discharge at 4 C to 2.0 V with a current cutoff of C/50. The voltage cutoffs used in this work follow those recommended by the manufacturer.

Our dataset is described in Supplementary Table 9. In total, our dataset consists of three 'batches', or cells run in parallel. Each batch has slightly different testing conditions. For the '2017-05-12' batch, the rests after reaching 80% SOC during charging and after discharging were 1 min and 1 s, respectively. For the '2017-06-30' batch, the rests after reaching 80% SOC during charging and after discharging were both 5 min. For the '2018-04-12' batch, 5 s rests were placed after reaching 80% SOC during charging, after the internal resistance test and before and after discharging.

A histogram of cycle life for the three datasets is presented in Supplementary Fig. 28. We note that four cells had unexpectedly high measurement noise and were excluded from analysis.

To standardize the voltage–capacity data across cells and cycles, all 4 C discharge curves were fitted to a spline function and linearly interpolated (Supplementary Fig. 29). Capacity was fitted as a function of voltage and evaluated at 1,000 linearly spaced voltage points from 3.5 V to 2.0 V. These uniformly sized vectors enabled straightforward data manipulations such as subtraction.

**Machine-learning model development.** This study involved both model fitting (setting the coefficient values) and model selection (setting the model structure). To perform these tasks simultaneously, a regularization technique was employed. A linear model of the form

$$\hat{y}_i = \hat{\mathbf{w}}^T \mathbf{x}_i \quad (1)$$

was proposed, where  $\hat{y}_i$  is the predicted number of cycles for battery  $i$ ,  $\mathbf{x}_i$  is a  $p$ -dimensional feature vector for battery  $i$  and  $\hat{\mathbf{w}}$  is a  $p$ -dimensional model coefficient vector. When applying regularization techniques, a penalty term is added to the least-squares optimization formulation to avoid overfitting. Two regularization techniques, the lasso<sup>66</sup> and the elastic net<sup>68</sup>, simultaneously perform model fitting and selection by finding sparse coefficient vectors. The formulation is

$$\hat{\mathbf{w}} = \operatorname{argmin}_{\mathbf{w}} \|\mathbf{y} - \mathbf{X}\mathbf{w}\|_2^2 + \lambda P(\mathbf{w}) \quad (2)$$

where the argmin function represents finding the value of  $\mathbf{w}$  that minimizes the argument,  $\mathbf{y}$  is the  $n$ -dimensional vector of observed battery lifetimes,  $\mathbf{X}$  is the  $n \times p$  matrix of features, and  $\lambda$  is a non-negative scalar. The first term

$$\|\mathbf{y} - \mathbf{X}\mathbf{w}\|_2^2 \quad (3)$$

is found in ordinary least squares. The formulation of the second term,  $P(\mathbf{w})$ , depends on the regularization technique being employed. For the lasso,

$$P(\mathbf{w}) = \|\mathbf{w}\|_1, \quad (4)$$

and for the elastic net,

$$P(\mathbf{w}) = \frac{1-\alpha}{2} \|\mathbf{w}\|_2^2 + \alpha \|\mathbf{w}\|_1 \quad (5)$$

where  $\alpha$  is a scalar between 0 and 1. Both formulations will result in sparse models. The elastic net has been shown to perform better when  $p \gg n$ <sup>68</sup>, as is often the case in feature engineering applications, but requires fitting an additional hyperparameter ( $\alpha$  and  $\lambda$ , as opposed to only  $\lambda$  in the lasso). The elastic net is also preferred when there are high correlations between the features, as is the case in this application. To choose the values of the hyperparameters, we apply four-fold cross-validation and Monte Carlo sampling.

The model development dataset is divided into two equal sections, referred to as the training and primary testing sets. These two sections are chosen such that each spans the range of cycle lives (see Supplementary Table 9). The training data are used to choose the hyper-parameters  $\alpha$  and  $\lambda$  and determine the values of the coefficients,  $\mathbf{w}$ . The training data are further subdivided into calibration and validation sets for cross-validation. The primary test set is then used as a measure of generalizability. The secondary test dataset was generated after model development.

RMSE and average percentage error are chosen to evaluate model performance. RMSE is defined as

$$\operatorname{RMSE} = \sqrt{\frac{1}{n} \sum_{i=1}^n (y_i - \hat{y}_i)^2} \quad (6)$$

where  $y_i$  is the observed cycle life,  $\hat{y}_i$  is the predicted cycle life and  $n$  is the total number of samples. The average percentage error is defined as

$$\% \operatorname{err} = \frac{1}{n} \sum_{i=1}^n \frac{|y_i - \hat{y}_i|}{y_i} \times 100 \quad (7)$$

where all variables are defined as above.

To summarize our procedure, we first divide the data into training and test sets. We then train the model on the training set using the elastic net, yielding a linear model with downselected features and coefficients. Finally, we apply the model to the primary and secondary test sets.

The data processing and elastic net prediction is performed in MATLAB, while the classification is performed in Python using the NumPy, pandas and sklearn packages.

## Data availability

The datasets used in this study are available at <https://data.matr.io/1>.

## Code availability

Code for data processing is available at <https://github.com/rdbraatz/data-driven-prediction-of-battery-cycle-life-before-capacity-degradation>. Code for the modelling work is available from the corresponding authors upon request.

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### Author contributions

P.M.A., N.J., N.P., M.H.C. and W.C.C. conceived of and conducted the experiments. K.A.S., Z.Y. and B.J. performed the modelling. M.A., Z.Y. and P.K.H. performed data management. P.M.A., K.A.S., N.J., B.J., D.F., M.Z.B., S.J.H., W.C.C. and R.D.B. interpreted the results. All authors edited and reviewed the manuscript. W.C.C. and R.D.B. supervised the work.

### Competing interests

K.A.S., R.D.B., W.C.C., P.M.A., N.J., S.J.H. and N.P. have filed a patent related to this work: US Application No. 62/575,565, dated 16 October 2018.

### Additional information

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